Tools and Techniques for Prototyping Haptic Interfaces Sensors and Sensor Processing



General Robotics, Automation, Sensing, and Perception Lab (GRASP) MEAM Department, SEAS, University of Pennsylvania



Haptics Symposium 2012 Workshop

Senses a physical quantity from the user, such as motion or force

Senses a physical quantity from the user, such as motion or force

Physically acts on the user via a variable actuator

Senses a physical quantity from the user, such as motion or force

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Connects sensing to acting with fast processing

Senses a physical quantity from the user, such as motion or force

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Connects sensing to acting with fast processing

it's all about physical interaction with a user...

it's all about physical interaction with a user...



it's all about physical interaction with a user...



Tactile Devices

Stimulate skin to create contact sensations



Tactile Devices

Stimulate skin to create contact sensations



Kinesthetic Devices

Apply forces to guide or inhibit body movement



Tactile Devices

Stimulate skin to create contact sensations



Attempt to combine tactile and kinesthetic feedback

Kinesthetic Devices

Apply forces to guide or inhibit body movement



Tactile Devices

Stimulate skin to create contact sensations



Hybrid Devices

Attempt to combine tactile and kinesthetic feedback

Kinesthetic Devices

Apply forces to guide or inhibit body movement

PHANTor

Measure tool tip position vector (possibly with orientation)

PHANTot

Measure tool tip position vector (possibly with orientation) Output force vector at tool tip

PHANToM

Measure tool tip position vector (possibly with orientation) Output force vector at tool tip Cycle at 1000 Hz

Typical Components of Kinesthetic Haptic Interfaces

Typical Components of Kinesthetic Haptic Interfaces



Capstan & Cable Drive Stiff Metal Linkages



Incremental Optical Encoder



Brushed Permanent Magnet Direct Current Motor



Current Amplifier



Computer Interface Card



K. J. Kuchenbecker and G. Niemeyer. Modeling induced master motion in force-reflecting teleoperation. In Proc. IEEE International Conference on Robotics and Automation, pages 348–353, Apr. 2005.

Elements of Haptic Interfaces

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Course Notes for MEAM 625, University of Pennsylvania Adapted from Section 3.1 of Professor Kuchenbecker's Ph.D. thesis [3].

A haptic interface plays the important role of connecting the user to the controller during interactions with remote and virtual objects. Such systems incorporate mechanical, electrical, and computational elements, which all interact to create the touch-based sensations experienced by the user. This document is concerned specifically with actuated impedance-type interfaces, which currently dominate the field due to their excellent free-space characteristics and their widespread use in a variety of applications. During an interaction, the controller of an impedance-type device must measure the user's hand motion and apply an appropriate force in response. Impedance-type haptic interfaces vary in design, but they usually include a series of electrical and mechanical elements between the handle and the computer, as described below.

Overview

Haptic interfaces typically provide two or three degrees of freedom in position, sensing the user's motion and applying feedback forces within this workspace. Many devices also permit changes in the orientation of the end effector; these rotational degrees of freedom can be unsensed, sensed but not actuated, or sensed and actuated. The remainder of this discussion will focus on translation rather than orientation, though the described design features can be applied to either.

Figure 1 illustrates the chain of elements typically present in each axis of a haptic interface. For clarity, the illustration depicts a device with a single degree of freedom, but typical systems combine several degrees of freedom in parallel or series to allow unrestricted translation and/or orientation. Although differences exist, individual position axes of most mechanisms can be represented by such an arrangement. The terms "haptic interface" and "master" are often used interchangeably to represent all electrical and mechanical elements depicted in Figure 1, extending from the amplifier and encoder to the handle.

1



This is just one way to build a haptic interface....

This is just one way to build a haptic interface....

There are many other approaches in the literature, and there are many still to be discovered.

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Physically acts on the user via a variable actuator

Connects sensing to acting with fast processing

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- Sensor Specifications
- Sensor Types
- Read the Datasheet





- Sensor Specifications
- Sensor Types
- Read the Datasheet



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- Sensor Specifications
- Sensor Types
- Read the Datasheet





ANALOG DEVICES

Small and Thin $\pm 18 g$ Accelerometer

ADXL321

FEATURES

Small and thin 4 mm × 4 mm × 1.45 mm LFCSP package 3 mg resolution at 50 Hz Wide supply voltage range: 2.4 V to 6 V Low power: 350 µA at V₅ = 2.4 V (typ) Good zero g bias stability Good sensitivity accuracy X-axis and Y-axis aligned to within 0.1° (typ) BW adjustment with a single capacitor Single-supply operation 10,000 g shock survival Compatible with Sn/Pb and Pb-free solder processes

APPLICATIONS

Vibration monitoring and compensation Abuse event detection Sports equipment

GENERAL DESCRIPTION

The ADXL321 is a small and thin, low power, complete dualaxis accelerometer with signal conditioned voltage outputs, which is all on a single monolithic IC. The product measures acceleration with a full-scale range of $\pm 18~g$ (typical). It can also measure both dynamic acceleration (vibration) and static acceleration (gravity).

The ADXL321's typical noise floor is $320 \,\mu g/\sqrt{Hz}$, allowing signals below 3 mg to be resolved in tilt-sensing applications using narrow bandwidths (<50 Hz).

The user selects the bandwidth of the accelerometer using capacitors C_X and C_Y at the X_{OUT} and Y_{OUT} pins. Bandwidths of 0.5 Hz to 2.5 kHz may be selected to suit the application.

The ADXL321 is available in a very thin 4 mm \times 4 mm \times 1.45 mm, 16-lead, plastic LFCSP.

FUNCTIONAL BLOCK DIAGRAM



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					ADXL321			
SPECIFICATIONS ¹								
$T_A = 25^{\circ}$ C, $V_S = 3$ V, $C_X = C_Y = 0.1 \mu$ F, Acceleration = 0 g, unless otherwise noted.								
Table 1.								
Parameter	Conditions	Min	Тур	Max	Unit			
SENSOR INPUT	Each axis		<i>,</i> ,					
Measurement Range			±18		q			
Nonlinearity	% of full scale		±0.2		%			
Package Alignment Error			±1		Degrees			
Alignment Error	X sensor to Y sensor		±0.1		Degrees			
Cross Axis Sensitivity			±2		%			
SENSITIVITY (RATIOMETRIC) ²	Each axis							
Sensitivity at Xout, Yout	$V_S = 3 V$	51	57	63	mV/g			
Sensitivity Change due to Temperature ³	$V_S = 3 V$		0.01		%/°C			
ZERO g BIAS LEVEL (RATIOMETRIC)	Each axis							
0 g Voltage at Xout, Yout	$V_S = 3 V$	1.4	1.5	1.6	V			
0 g Offset vs. Temperature			±2		mg/°C			
NOISE PERFORMANCE								
Noise Density	@ 25°C		320		µg/√Hz rms			
FREQUENCY RESPONSE ⁴								
C _X , C _Y Range ⁵		0.002		10	μF			
R _{FILT} Tolerance			32 ± 15%		kΩ			
Sensor Resonant Frequency			5.5		kHz			
SELF-TEST ⁶								
Logic Input Low			0.6		v			
Logic Input High			2.4		v			
ST Input Resistance to Ground			50		kΩ			
Output Change at Xout, Yout	Self-test 0 to 1		18		mV			
OUTPUT AMPLIFIER								
Output Swing Low	No load		0.3		V			
Output Swing High	No load		2.6		V			
POWER SUPPLY								

2.4

-20

V

mΑ

ms

°C

6

+70

0.49

20

¹ All minimum and maximum specifications are guaranteed. Typical specifications are not guaranteed.

² Sensitivity is essentially ratiometric to V_s.

Operating Temperature Range

Operating Voltage Range

Quiescent Supply Current

Turn-On Time⁷

TEMPERATURE

³ Defined as the change from ambient-to-maximum temperature or ambient-to-minimum temperature. ⁴ Actual frequency response controlled by user-supplied external capacitor (C_x , C_y). ⁵ Bandwidth = 1/($2 \times \pi \times 32 \text{ k}\Omega \times C$). For C_x , $C_y = 0.002 \text{ }\mu\text{F}$, bandwidth = 2500 Hz. For C_x , $C_y = 10 \text{ }\mu\text{F}$, bandwidth = 0.5 Hz. Minimum/maximum values are not tested.

⁶ Self-test response changes cubically with V_s.

⁷ Larger values of C_x, C_Y increase turn-on time. Turn-on time is approximately 160 × C_x or C_Y + 4 ms, where C_x, C_Y are in µF.

Rev. 0 | Page 3 of 16

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OUTPUT AMPLIFIER					
Output Swing Low	No load		0.3		V
Output Swing High	No load		2.6		V
POWER SUPPLY					
Operating Voltage Range		2.4		6	V
Quiescent Supply Current			0.49		mA
Turn-On Time ⁷			20		ms
TEMPERATURE					
Operating Temperature Range		-20		+70	℃
Each axis					
---------------------------	---	--	--	---	
		±18		g	
% of full scale		±0.2		%	
		±1		Degrees	
X sensor to Y sensor		±0.1		Degrees	
		±2		%	
Each axis					
$V_{\rm S} = 3 V$	51	57	63	mV/ <i>g</i>	
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@ 25°C		320		µg/√Hz rms	
	0.002		10	μF	
		32 ± 15%		kΩ	
		5.5		kHz	
		0.6		V	
		2.4		V	
		50		kΩ	
Self-test 0 to 1		18		mV	
No load		0.3		V	
No load		2.6		V	
	2.4		6	V	
		0.49		mA	
		20		ms	
	-20		+70	°C	
	Each axis % of full scale X sensor to Y sensor Each axis $V_S = 3 V$ $V_S = 3 V$ Each axis $V_S = 3 V$ @ 25°C Self-test 0 to 1 No load No load	Each axis% of full scaleX sensor to Y sensorEach axis $V_5 = 3 V$ $V_5 = 3 V$ Each axis $V_5 = 3 V$ 1.4@ 25°C0.002Self-test 0 to 1No loadNo loadNo load2.4	Each axis ± 18 % of full scale ± 0.2 X sensor to Y sensor ± 0.1 ± 2 Each axis $V_5 = 3 V$ 51 $V_5 = 3 V$ 51 $V_5 = 3 V$ 1.4 $V_5 = 3 V$ 1.4 $\psi_5 = 3 V$ 0.002 0.002 $32 \pm 15\%$ 0.002 $32 \pm 15\%$ 5.5 0.66 2.4 50 Self-test 0 to 1 18 No load 0.3 No load 2.6 2.4 0.49 20 -20	Each axis ± 18 % of full scale ± 0.2 ± 1 ± 0.2 ± 1 ± 0.1 ± 2 ± 0.1 Each axis 0.1 $V_5 = 3 V$ 51 57 63 $V_5 = 3 V$ 0.01 0.01 1.6 Each axis $V_5 = 3 V$ 1.4 1.5 1.6 $\psi_5 = 3 V$ 1.4 1.5 1.6 (0.002) 10 $32 \pm 15\%$ 5.5 (0.002) 10 $32 \pm 15\%$ 5.5 0.06 2.4 50 5.5 Self-test 0 to 1 18 1.8 1.8 No load 0.3 2.6 2.4 6 0.49 20 20 -20 $+70$	

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Sensor Specifications



Static Measures

- <u>Range</u>: minimum to maximum of measurable physical quantity, e.g., 10-20 PSI
- <u>Span</u>: the limits between minimum and maximum value the sensor can measure
- Error: measured value minus true value, often associated with a specific cause
- Accuracy: total of the effects of all errors
- <u>Sensitivity:</u> Gain (output divided by input), may be ratiometric with supply voltage

Dynamic Measures

- Response Time time to achieve 95% of final value
- <u>Time Constant</u> time to achieve 63% of final value
- <u>Rise time</u> time from 10% to 90% of final value
- <u>Settling time</u> time to get and stay within 2% of final value



Imperfections



- Hysteresis: Sensitivity to direction of change
- <u>Nonlinearity</u>: deviation from linear relationship (constant gain)
- <u>Repeatability</u>: produces the same output for the same input (not the same as accuracy)
- <u>Stability</u>: holding the same value over a period of time
- <u>Deadband/Dead Time</u>: period or range of input where no output occurs
- <u>Resolution</u>: Smallest change in input that will cause a change in output
- <u>Output Impedance</u>: ability to deliver current, lower is better







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Sensor Types



• All convert a physical effect into an electrical signal



Sensor Types



- All convert a physical effect into an electrical signal
 - Measure a voltage or current using capacitance, resistance, inductance





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 - Size





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 - May output analog voltage, digital signal, serial comm., current, etc.
- Choosing a sensor is always about:
 - Cost
 - Size
 - Accuracy





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- Choosing a sensor is always about:
 - Cost
 - Size
 - Accuracy
 - Durability
 - Availability
 - Compatibility with rest of system (interference, communication)
 - Other concerns?

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Mechanical Trackers



- Ground-based linkages most commonly used
- Position Sensors
 - Analog: potentiometers or Hall-effect (magnetic)
 - Digital: encoders (optical or MR)

Adapted from slides by Will Provancher



Potentiometers





- Typically rotary, but linear exist.
- Cheap and easy.
- Moving parts means it can wear out.
- Hard to waterproof or dustproof.
- Has non-negligible friction.

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Hall-Effect Sensors



- How do they work?
 - A <u>small transverse voltage</u> is generated across a current-carrying conductor <u>in the presence of a</u> <u>magnetic field</u>



(Discovery made in 1879, but not useful until the advent of semiconductor technology)

Adapted from slides by Will Provancher

Hall-Effect Sensors $V_{h} = \frac{R_{h}IB}{t}$

 V_h = Hall voltage

- R_h = Hall coefficient
- I = Current
- B = Magnetic flux density
- *t* = Element thickness
- Amount of voltage output related to the strength of magnetic field passing through.
- Linear over small range of motion
 - Need to be calibrated
- Affected by temperature, other magnetic objects in the environments



Hall-Effect Sensors



- V_h = Hall voltage
- R_h = Hall coefficient
- I = Current
- B = Magnetic flux density
- *t* = Element thickness



 The voltage varies sinusoidally with rotation angle

Adapted from slides by Will Provancher









Some material adapted from slides by A. Okamura and W. Provancher



Some material adapted from slides by A. Okamura and W. Provancher



rotation

axis

Optical Disk

- The most common motion sensor in haptics is the incremental optical encoder, often by Agilent.
- A thin disk is attached to the rotating shaft whose angle you want to measure, usually the motor.





- A thin disk is attached to the rotating shaft whose angle you want to measure, usually the motor.
- The disk has slits cut into it in a regular pattern.





- A thin disk is attached to the rotating shaft whose angle you want to measure, usually the motor.
- The disk has slits cut into it in a regular pattern.
- A light shines on the disk on one side, and photo sensors are located on the opposite side.





- A thin disk is attached to the rotating shaft whose angle you want to measure, usually the motor.
- The disk has slits cut into it in a regular pattern.
- A light shines on the disk on one side, and photo sensors are located on the opposite side.
- Produces a number of pulses per revolution, with higher resolution being more expensive.



Some material adapted from slides by A. Okamura and W. Provancher















Some material adapted from slides by A. Okamura and W. Provancher



LED/Photodiode

Encoder Parts

reader

rotation

axis

Optical Disk



• The system has no knowledge of absolute position, because it's always just counting pulses.





- The system has no knowledge of absolute position, because it's always just counting pulses.
- How can you solve this?





- The system has no knowledge of absolute position, because it's always just counting pulses.
- How can you solve this?
 - Calibration pose (SensAble)




- The system has no knowledge of absolute position, because it's always just counting pulses.
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 - Secondary sensors with absolute readings (da Vinci)





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- Sometimes problems occur at high velocities.





- The system has no knowledge of absolute position, because it's always just counting pulses.
- How can you solve this?
 - Calibration pose (SensAble)
 - Secondary sensors with absolute readings (da Vinci)
- Sometimes problems occur at high velocities.
- No noise on position, but uncertainty due to resolution, and significant noise on velocity.





- The system has no knowledge of absolute position, because it's always just counting pulses.
- How can you solve this?
 - Calibration pose (SensAble)

$$\theta_m = \Delta(Q - Q_{zero})$$

- Secondary sensors with absolute readings (da Vinci)
- Sometimes problems occur at high velocities.
- No noise on position, but uncertainty due to resolution, and significant noise on velocity.



LVDT



- Linear variable displacement transducer
- Very accurate
- More complex to support than potentiometers or encoders – need multiple AC voltage sources
- Inherently analog





Proximity Sensors

- Implies that one only wants data when something is close – don't care when it is "far away"
 - Eddy current proximity sensor lower accuracy
 - Inductive proximity sensor senses metallic objects
 - Limit switch rugged sealed on/off designed for repeated contact with moving parts
 - Infrared emitter-detector pair reflected IR from source gives indication of distance
 - Ultrasonic range sensor reflected ultrasonic signal from source gives indication of distance





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Switches



- Rotary, pushbutton, slide, toggle, tilt ...
- Momentary vs. Persistent ON/OFF
- Many, many types
- Bounce



Videos from http://video_demos.colostate.edu/mechatronics/

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Switches



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Light

GND



- Photodiodes, phototransistors, photoresistors
 - Small, easy to fit into electronic systems.
 - Require electrical engineering knowledge to implement properly.
 - Can set up in a variety of ways, including distance reflectance, gray-scale reflectance, distance intensity, break beam

- Ambient light can impact performance.



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Strain Gauges



- Change in length changes resistance
- Temperature also changes
 resistance





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Force Sensing



- Measure the position change on an elastic element
- Strain gauge load cell clever layout of gauges & material shape to create accurate system
- Fluid pressure on a diaphragm measure change in length/size of a diaphragm with strain gauges
- Piezo electric crystals generate electrical signals when a strain is generated – typically used for high frequency force PI changes (accelerations)







A single ended compression accelerometer



A load cell



 A piece of metal that is designed to deform in a predictable way to create a measurement of load (torque and/or force)



Adapted from slides by John Morrell

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Force Sensors

- How do they work?
 - Typically a flexure + a strain gage (sometimes also piezoelectric sensors, but these tend to drift)
- A good quality 6-axis forcetorque sensor is ~\$6000
 - Mechanically delicate do not drop or hit
 - Sensitive to temperature fluctuations

6-Axis JR3 Force Torque Load Cell





JR3.com

ATI Nano17 Transducer



www.ati-ia.com

Force Sensing Resistors

Known as FSRs

- Piezoresistive ink
- Tons of sensor drift and hysteresis, sensitivity to contact location
- Very thin!
- Cheap ~\$10
- Use drive circuit recommended by manufacturer to get voltage output that is approximately linear with force



Interlink FSR



www.interlinkelectronics.com

Tekscan Flexiforce FSR



Adapted from slides by Will Provancher



Temperature



- Thermistor
- RTD
- Thermocouples
- Equations vary but they are all nonlinear and require some "figuring" to get the right answer



Typical RTD Design





Inertial Sensing

Inertial Sensing

00	MEMS Inertial Sensors MEM	MS and Sensors Analog Devices	
Image: A the second	og.com/en/mems-sensors/mems-inertial	-sensors/products/index.html C Q- Google	9
WORLD LEADER IN	HIGH PERFORMANCE	SIGNAL PROCESSING Select a Language: English	
ANALOG DEVICES Enter keyw	vords or part # Search	Parametric Cross-Reference and Log In Product Search Obsolete Search	
PRODUCTS APPLICATI	ONS RESOURCES & TOOLS	SAMPLE & PURCHASE SUPPORT WAnalog	
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		ADIS16488 - Low Profile, Low Noise Ten Degrees of Freedom Inertial Sensor	
		ADXL337 - Small, Low Power, 3-Axis ±3 g Accelerometer	
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Sensor MEMS Inertial Measurement Units MEMS Gyroscopes		Industrial Platform	
		Chabinzation Oyotemio	
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Sense Acceleration	Sense Tilt	Sense Rotation Sense Shock	Ţ

Inertial Sensing



MEMS-based Accelerometers



MEMS-based Accelerometers







Measures acceleration and gravity



MEMS-based Rate Gyroscopes



MEMS-based Rate Gyroscopes



MEMS-based Rate Gyroscopes



Measures angular velocity

Inertial Measurement Units (IMUs)

9 Degrees of Freedom on a single, flat board for \$125:

ITG-3200 - triple-axis digitaloutput gyroscope

ADXL345 - 13-bit resolution, ±16g, triple-axis accelerometer

HMC5883L - triple-axis, digital magnetometer

Outputs of all sensors processed by on-board ATmega328 and sent out via a serial stream



Inertial Measurement Units (IMUs)



Same sensors in a clean package with all processing and software done for you, estimates absolute heading, around \$2000?

Magnetic Tracking





Field generator creates magnetic field; small wired sensors used to estimate position and orientation of tracked item; bad interference from metal and electromagnetic actuators; price ranges from ~\$300 (Razer Hydra) to ~\$16,000 (precise, medical use).



Custom camera system with blob detection in 2D; limited by camera frame rate, processing time



VICON system, many cameras, passive markers, >\$100k





OptoTrak system: 3 cameras, active markers, ~\$50k?





WiiMote camera: finds 4 brightest IR spots, ~\$40







Kinect: color camera with depth, tracks humans, ~\$200









Mouse Sensor: senses optical flow in 2D, digital comm.



Sensor Videos





Videos from http://video_demos.colostate.edu/mechatronics/

Yale Mechanical Engineering


Sensor Videos



	Video Demonstrations of Mechatronics Principles	
▲▶@+	Mttp://video_demos.colostate.edu/mechatronics/	Q- Google
158. auton	obile automatic wiper and defroster (2.6 MB)	
159. card o	lealer (4.5 MB)	
160. <u>alarm</u>	clock (2.5 MB)	
161. auton	ated ice-fishing pole (2.7 MB)	
162. <u>subm</u>	ersible temperature and pressure sensor apparatus (3.9 MB)	
163. motor	indexer (1.4 MB)	
• power tran	smission	
• high	voltage power transmission line cables and connectors (2.2 MB)	
• high	voltage disconnect switch (0.6 MB)	
 powe 	r station transformer fire (photos during, close-up, and after)	
• zappe	d squirrel (and stupid man)	
 sensors 		
 accele 	crometer bearing signature analysis experiment (3.3 MB)	
 bound 	ting ball accelerometer (0.7 MB)	
• comp	uter mouse relative encoder (1.0 MB)	
• EMG	sensor used to control a robot (6.0 MB)	
• encod	er components (1.8 MB)	
 infrar 	ed proximity sensor used in an automated laboratory rat exercise machine (8.0 MB)	
 inkjet 	printer components with custom digital encoders (6.8 MB)	
• <u>LVD</u>	r principles of operation	
• <u>magn</u>	etic pickup tachometer used in a PID speed controller test-stand (4.0 MB)	
• <u>magn</u>	etostrictive position sensor (0.8 MB)	
 robot 	digital encoder components (4.3 MB)	
•	see also: Adept One robot internal design and construction (4.6 MB)	
• <u>strain</u>	gage rosette experiment (2.4 MB)	
•	strain gage rosette experiment analysis discussion (10.3 MB)	
•	PDF file containing analysis summary	
• <u>switc</u>	<u>nes</u> (1.6 MB)	
• <u>switc</u>	<u>a bounce</u> (0.8 MB)	
• therm	ocouple with a digital thermometer (4.5 MB)	
• therm	ostat with bimetallic strips and mercury switch (2.3 MB)	
• <u>voice</u>	<u>coil</u> (1.1 MB)	

Videos from http://video_demos.colostate.edu/mechatronics/

Yale Mechanical Engineering

Adapted from slides by John Morrell

Quick Quiz What sensors do you see?

Nitinol Strip

Linear Stage

Image from Marayong, Na, and Okamura (ICRA 2007)

Quick Quiz What sensors do you see?

Encoder



Image from Marayong, Na, and Okamura (ICRA 2007)

Any other types of sensors you are wondering about?

Sensor Processing



Illustration from K. J. Kuchenbecker and G. Niemeyer, "Induced Master Motion in Force-Reflecting Teleoperation." ASME Journal of Dynamic Systems, Measurement, and Control. Volume 128(4):800-810, December 2006.



Illustration from K. J. Kuchenbecker and G. Niemeyer, "Induced Master Motion in Force-Reflecting Teleoperation." ASME Journal of Dynamic Systems, Measurement, and Control. Volume 128(4):800-810, December 2006.

Typical Software Configuration

Input: from sensor signals to counts



D/A and A/D

- Converts between voltages and counts
- Computer stores information digitally, and communicates with the outside world using signed voltage signals
 - e.g., for 8-bit 0-5V ADC
 2.5V = 10000000

_SB

Adapted from slides by Will Provancher

MSB



Decimal	Binary	Hexadecimal
0	0000	0
1	0001	1
2	0010	2
3	0011	3
4	0100	4
5	0101	5
6	0110	6
7	0111	7
8	1000	8
9	1001	9
10	1010	А
11	1011	В
12	1100	С
13	1101	D
14	1110	E
15	1111	F





 Get counts Q_j from encoder counters, serial communications, or analog-to-digital conversions.



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- Convert counts to sensor shaft angles θ_{sj} or sensor displacements d_{sj} using knowledge of the sensor's characteristics.



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- Convert sensor angles to joint coordinates q_j (joint angles θ_j or joint displacements d_j) using the gear ratio. In this process, use a negative sign to flip the joint angle direction if desired.



$$\vec{q}_k = \vec{a} * \vec{Q}_k + \vec{b}$$

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$$\vec{q}_k = \vec{a} * \vec{Q}_k + \vec{b}$$



Input Processing: from counts to joint values

$$\vec{q}_k = \vec{a} * \vec{Q}_k + \vec{b}$$

• Check your work along the way.



$$\vec{q}_k = \vec{a} * \vec{Q}_k + \vec{b}$$

- Check your work along the way.
- How?



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 - Units



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- Check your work along the way.
- How?
 - Units
 - Known configurations



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- How?
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 - Ranges



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- Check your work along the way.
- How?
 - Units
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 - Record and graph



$$\vec{q}_k = \vec{a} * \vec{Q}_k + \vec{b}$$

- Check your work along the way.
- How?
 - Units
 - Known configurations
 - Ranges
 - Record and graph
- Check before you use the movement information to output forces.

Digital differentiation

- Many different methods
- Simple Example:
 - Position reading at time 1 = P1
 - Position reading at time 2 = P2
 - t is the period of the servo loop (in sec. or counts)
 - The position is typically sampled on a fixed interval
- Differentiation increases noise





V = P2 - P1

Noisy Velocity readings



- Noise on velocity signal can create jitter on your haptic device when your controller has velocity feedback (virtual damping)
- Common solutions
 - Use a Tach/Generator
 - Voltage goes with speed (same source as back-EMF)
 - Resolution is set by your A/D converter
 - Integrate the signal from an accelerometer
 - Measure time per tick rather than ticks per time
 - Use a special chip that measures time between ticks
 - Especially good to do at slow speeds
 - Fares poorly at high velocities
 - Filtering (conventional to smooth or Kalman filtering to combine sensor signals)

Adapted from slides by Will Provancher

Calculating Velocity

Calculating Velocity

hapticCallback()

Main callback that sets the force that the user will feel. It gets the current position and velocity of the device.

This is what you want to edit to change the system's haptic feedback.

HDCallbackCode HDCALLBACK hapticCallback(void *data)

// Local variables.

{

```
hduVector3Dd position;
hduVector3Dd velocity;
hduVector3Dd force;
hduVector3Dd extraForce;
hduVector3Dd proxyPosition;
HDint currentButtonState;
HDint lastButtonState;
double stiffness = 0.25; // Units are newtons per millimeter.
```

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```

// Local variables for custom velocity calculation.
static bool firstTime = true;
static hduVector3Dd lastPosition; // mm
hduVector3Dd rawVelocity; // mm/s
static hduVector3Dd filteredVelocity(0.0, 0.0, 0.0); // mm/s
float filterWeight = 0.03;
float dampingCoefficient = 0.01; // N/(mm/s)
hduVector3Dd dampingForce; // N

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hduVector3Dd dampingForce; // N

```
// Get the handle for the current haptic device.
HHD hHD = hdGetCurrentDevice();
```

// Begin the haptic frame for this device.
hdBeginFrame(hHD);

// Get its position and velocity and store them in hduVector3Dd variables. hdGetDoublev(HD_CURRENT_POSITION, position); // Units are millimeters. hdGetDoublev(HD_CURRENT_VELOCITY, velocity); // Units are millimeters per second.

```
// Fill lastPosition with current position if this is the first function call.
if (firstTime) {
   lastPosition = position;
   firstTime = false;
}
```

// Calculate the raw velocity from this position and lastPosition.
rawVelocity = (position - lastPosition) / DELTAT;

```
// Low-pass filter this raw velocity signal using a first-order IIR filter.
filteredVelocity = filterWeight * rawVelocity + (1 - filterWeight) * filteredVelocity;
```

```
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hdGetDoublev(HD_CURLENT are control of this are millimeters per second.
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```

// Store current position as lastPosition for next time.
lastPosition = position;

// Use the custom filtered velocity rather than SensAble's velocity?
// Comment out this line if you want to use the standard velocity.
velocity = filteredVelocity;

```
// Compute an extra damping force to add to the force the user feels,
// just so you can test the velocity.
dampingForce = -dampingCoefficient * velocity;
```

// Other code....

```
// Compute the force.
force = stiffness * (proxyPosition - position) + dampingForce + extraForce;
```

$$v_{smooth}(k) = w \cdot v_{raw}(k) + (1 - w) \cdot v_{smooth}(k - 1)$$












Begin with a first-order continuous time low-pass filter, where Y(5) is the Laplace transform of the filtered subput and X(s) is that of our signal. € gain = 1@ 5=0 output > Y (5) 2 X(5) 5+2 input 1 one pole at -2, 2 is filter autoffin mad/s Convert from continuous time (smooth derivatives) to discrete time (sampled at intervals of Tseconds). This requires us to choose a method for approximating the derivative. Other options would work too, but the simplest is tackward differencing : Z transform acts like a shift operator. $(1 - \overline{z})$ $Y(z) * \overline{z}'$ is previous y value 5 Substitute this in for 3 in the above eqn. makessense: $Y(z) \frac{1}{2}$ $Y(z) \frac{1}{2}$ Y(z) * z° = Y(z) is this yvalue > do inverse = transform $y(k) = \frac{2T}{1+2T} \times (k) + \frac{1}{1+2T} y(k-1)$ indux $Y(z)\left[\frac{(1-z^{-1})}{T}+\lambda\right] = \lambda X(z)$ $\gamma(k) = w \cdot \chi(k) + (1 - w) y(k - 1)$ $Y(z) - Y(z) * z^{-} + \lambda T Y(z) = \lambda T X(z)$ filter-weight = $\frac{2T}{1+2T}$ $(1+\lambda T)Y(z) = \lambda T X(z) + z' * Y(z)$ $Y(z) = \frac{2T}{1+2T} X(z) + \frac{1}{1+2T} z'Y(z) - \frac{1}{1+2T} z'Y(z)$

$$\lambda = \frac{w}{T(1-w)}$$

$$\lambda = \frac{w}{T(1-w)} \qquad \qquad f = \lambda \cdot \frac{1 \text{ cycle}}{2\pi \text{ rad}} = \frac{w}{T(1-w)} \cdot \frac{1 \text{ cycle}}{2\pi \text{ rad}}$$



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hduVector3Dd dampingForce; // N

A sample custom haptic device







Motor with Gearhead and Digitial Encoder











Motor with Gearhead and Digitial Encoder









orce/Torque Sensor

























 $\tau_m = k_p(\theta_d - \theta_m) + k_d(\omega_d - \omega_m)$

 $\tau_m = k_p(\theta_d - \theta_m) + k_d(\omega_d - \omega_m)$

































-(DOS)-- knob_07_01_05.cpp 24% L333 (C++ Abbrev)-------

```
Haptic_Function
        This is the function that updates the system's forces
 ******
void __stdcall Haptic_Function(void *pv)
£
        int i:
        static double timer = 0; // Used as a timer for several different purposes.
        // *** TIMING ***
        // Cache the time of the previous haptic function call.
        lastTime = thisTime;
        // Find out what time it is now. This information facilitates accurate velocity calculation.
        QueryPerformanceCounter(&thisTime);
        // Calculate time since last call in clock cycles and then convert to seconds.
deltaTime.QuadPart = (thisTime.QuadPart - lastTime.QuadPart);
        deltaTimeS = (float) deltaTime.LowPart / (float) ticksPerSecond.QuadPart;
        // *** FORCE/TOROUE MEASUREMENTS ***
        // Get present voltage values from f/t sensor
        RawVoltage(tempRawVoltage);
        // Filter voltage
        for (i=0 ; i<7 ; i++) {
               filteredRawVoltage[i] = LowPass1((double)1.0/(2.0*PI*50.0), deltaTimeS, (double)tempRawVol
⊈tage[i], (double)filteredRawVoltage[i]);
        // Handle initialization of force/torque sensor
        if ((force_bias_initialize) && (filter_wait > 50))
               if (Number_of_Samples < MAX_NUMBER_OF_SAMPLES) {</pre>
                      for (int CONV_r = 0; CONV_r < 7; CONV_r++) {
                             VoltageBiasTemp[CONV_r][Number_of_Samples] = filteredRawVoltage[CONV_r];
                      Number_of_Samples++;
 -(DOS)-- knob_07_01_05.cpp 63% L918 (C++ Abbrev)-----
```

```
// *** MOTOR CONTROL ***
        // Save last position for velocity computation.
         lastPosDeg = curPosDeg;
         // Read in encoder signals from the QUAD04 board
         ULStat = cbCIn32 (QUAD_BOARD_NUM, MOTOR_ROT, &rot_cts);
         //Convert to signed counts
         rot_cts_signed = rot_cts;
        // Convert signed counts to degrees
         curPos = rot_cts_signed - LoadValue;
         curPosDeg = curPos / CTS_PER_DEG;
                                                                // Converts position to units of degrees
        // Check for freak position reads - if change is too much, discard this reading, and use the last ₽
sone.
         if (fabs(curPosDeg - lastPosDeg) > 1) {
                 curPosDeg = lastPosDeg;
 п
         // Compute velocity and low-pass filter.
         unfiltVelDeg = (curPosDeg - lastPosDeg) / deltaTimeS;
         curVelDeg = LowPass1(1/(2*PI*50), deltaTimeS, unfiltVelDeg, curVelDeg);
        // F/T transducer safety checks.
         if(fabs(FTValues[0])>200 || fabs(FTValues[1])>200 || fabs(FTValues[2])>500 || fabs(FTValues[3])>15₽
≤00 || fabs(FTValues[4])>1500 || fabs(FTValues[5])>2000) {
                 // If over limits, make desired position present position with no output.
                 desPosDeg = curPosDeg;
                 desVelDeg = curVelDeg;
                current = 0;
                voltage = 0;
        } else {
                 // Calculate the proxy's position and velocity during a trial for all of the different sta
•tes.
                 switch (state) {
                 case waitingForParameters:
                 case ready:
                        // Trial set will start soon. Keep proxy at zero position.
                        proxyPosDeg = 0;
                         proxyVelDeg = 0;
                         break;
                 case showingCommand:
                         // Next trial will start soon. Keep proxy at its current position, sitting still.
                         proxyPosDeg = proxyPosDeg;
                        proxyVelDeg = 0;
 -(DOS)** knob_07_01_05.cpp 69% L1001 (C++ Abbrev)-----
```

```
⊆otFeedback ? 'D' : 'd', proprioceptiveFeedback ? 'P' : 'p', tactileFeedback ? 'T' : 't', commandPosDeg, co⊇
smmandWidthDeg);
                 return;
         1/}
         // Output the desired values to the file.
         // Write parameters.
         fprintf(output_file, "subjectNumber = %d;\n\n", subjectNumber);
         fprintf(output_file, "setNumber = %d;\n\n", setNumber);
         fprintf(output_file, "trialNumber = %d;\n\n", trialNumber);
         fprintf(output_file, "lineFeedback = %d;\n\n", lineFeedback);
         fprintf(output_file, "dotFeedback = %d;\n\n", dotFeedback);
         fprintf(output_file, "proprioceptiveFeedback = %d;\n\n", proprioceptiveFeedback);
         fprintf(output_file, "tactileFeedback = %d;\n\n", tactileFeedback);
         fprintf(output_file, "commandPosition = %d;\n\n", commandPosDeg);
         fprintf(output_file, "commandWidth = %d;\n\n", commandWidthDeg);
         fprintf(output_file, "proxyAdmittance = %f;\n\n", proxyAdmittance);
         fprintf(output_file, "k = %f;\n\n", k);
         fprintf(output_file, "b = %f;\n\n", b);
П
         // Write the real time vector.
         fprintf(output_file, "clockTicksPerSecond = %I64d;\n\n", ticksPerSecond);
         fprintf(output_file, "tClock = [");
         for(i=0; i<dataIndex; i++) {</pre>
                 fprintf(output_file, "%I64d\t", timeArray[i]);
         fprintf(output_file, "]' - %I64d;\n", timeArray[0]);
         fprintf(output_file, "t = tClock / clockTicksPerSecond;\n\n");
         // Write time-varying data.
         fprintf(output_file, "dacVoltage = [");
         for(i=0; i<dataIndex; i++) {</pre>
                 fprintf(output_file, "%.9f\t", dacVoltageArray[i]);
         fprintf(output_file, "]';\n\n");
         fprintf(output_file, "fingerForce = [");
         for(i=0; i<dataIndex; i++) {</pre>
                 fprintf(output_file, "%.9f\t", fingerForceArray[i]);
         fprintf(output_file, "]';\n\n");
         fprintf(output_file, "motorPosition = [");
         for(i=0; i<dataIndex; i++) {</pre>
                 fprintf(output_file, "%.9f\t", motorPositionArray[i]);
         fprintf(output_file, "]';\n\n");
 -(DOS)-- knob_07_01_05.cpp 93% L1346 (C++ Abbrev)-------
```










Know your sensors and your signals.

Thank You



Questions?



kuchenbe@seas.upenn.edu http://haptics.grasp.upenn.edu